THz Test and Measurement Technology and Techniques

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Outline

- Introduction
 - Schottky Diode Technology
 - Solid-State THz Mixers & Multipliers
- THz Frequency Extension
 - Source Extenders
 - Spectrum Analyzer Extenders
- THz Vector Network Analysis
 - Waveguide Measurements
 - Quasi-optical Measurements
 - THz Wafer Probing
- Conclusions





Applications

- Spectroscopy
 - Imaging
- Communications

 Molecular Spectroscopy Radio Astronomy, Atmospheric • EPR/NMR/DNP • Plasma Diagnostics Weather Monitoring

General Test & Measurement



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7.5 7.505



Core Technology: Use nonlinear devices to extend the frequency range of traditional microwave electronics



Example: Triquint 2W 30-40 GHz Amp

- Chip developed for Radar and Satellite Communications
 - Chip size 2.5x3 mm
- The same chip can be used to drive THz multiplier chains
 - 2 W at 30-40 GHz
 - 0.75 W at 70 GHz
 - 200 mW at 140 GHz
 - etc...
- Microwave technology enables THz solid-state systems



Key Features

- 30 40 GHz Bandwidth
- > 33 dBm Nominal Psat @ Pin = 20dBm
- 18 dB Nominal Gain
- Bias: 6 V, 1050 mA Idq (1.9A under RF Drive)
- 0.15 um 3MI MMW pHEMT Technology



http://www.triquint.com/products/p/TGA4516-TS

Example: Herley-CTI Synthesizer

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- Fast-switching synthesizers
 - Very narrow linewidths
 - Hertz widths are possible even at THz
 - Allow narrowband filtering to reduce noise
 - 14 GHz → Phase noise -107 dBc/Hz @ 1 kHz offset
 - Compact and ruggedized
- THz multipliers can extend synthesizers to > 3 THz
 - Phase noise rises upon frequency multiplication by 20*log(N)
 - Can achieve excellent THz phase noise
 - e.g. 1 THz \rightarrow -70 dBc/Hz @ 1 kHz offset



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www.aspen-electronics.com/files/CTI/XS.pdf



Single sideband phase noise

www.telestrian.co.uk/phasenoise.html

Test & Measurement: Spectrum Analyzers

- Sophisticated instrument to analyze microwave signals
 - Spectral purity
 - Phase noise
 - Communication Signal Demodulation
- A core microwave test capability
 - Along with sources and vector network analyzers
- Can be extended to THz using the Schottky technology



Agilent PXA



Rohde & Schwarz FSU



Core Technology: Use nonlinear devices to extend the frequency range of traditional microwave electronics



Schottky Diodes

- Metal-semiconductor junction
 - Majority carrier device
 - Cutoff frequencies well into the THz
 - Room temperature operation
 - Improves with cooling
- Diode is well modeled by relatively simple quasi-static I-V and C-V equations
- Well-developed fabrication technology
 - Air-bridge used to reduce capacitance
 - Low capacitance is important for THz



 $I_d = I_{SAT} \left(e^{\left(\frac{V_j - I_d R_S}{V_0} \right)} \right)$



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VDI Planar Diode Fabrication Technology

- Planar Schottky Diodes
 - Mechanically rugged
 - Photolithographic reproducibility
- Integration of Diode with Coupling Circuitry
 - Operation to higher frequencies (>3 THz)
 - More repeatable assembly



Flip-chip Planar Diode





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Integrated Planar Diodes

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VDI Heterodyne Mixers



- Mixers available from WR-15 (50-75 GHz) to WR-0.4 (2-2.8 THz)
- Single & Anti-parallel Schottky mixers
 - Room temperature operation
 - Operation at High IF
- Full waveguide band design
 - Excellent Sensitivity
 - Tunerless
 - Planar & rugged



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VDI Mixer Performance Summary



Measured Performance of WR-6.5SHM



Schottky Diode Frequency Multipliers

- Careful choice of circuit configuration
 - Balanced design allows for broad bandwidth and high efficiency
 - Spatial mode filtering between harmonics
- Multiple diodes for increased power handling
- CAD Design to allow tunerless operation
 - First try success



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Balanced Circuit Topology



Porterfield et al (MTT, 1999)

Power from Multipliers



Recent High Power Multiplier Results

180 mW @ 224 GHz



3 uW @ 2.7 THz







Waveguide Based Components: Varactor Frequency Tripler



Porterfield, 2007 IMS Symp. Dig., pp. 337-340



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Rectangular Waveguide

- Why rectangular guide?
 - Low loss guiding structure at THz
 - Microstrip ~ 1 dB/mm @ 600 GHz
 - Waveguide ~0.08 dB/mm @ 600 GHz
 - High power handling
 - Many techniques for integration of device with guide



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www.ee.bilkent.edu.tr

Rectangular Waveguide – TE10 Mode

- Single-mode Operation
 - High pass filter
 - Blocks lower harmonics
 - Operate with only TE10 mode propagating
 - TE20 mode is next highest mode
 - Turns on at 2 times the TE10 cutoff frequency
 - Operating range approx. 1.25 to 1.9 times the TE10 cutoff frequency
 - To reduce the effect of dispersion on performance





Top View (TE $_{10}$)

____ Electric field lines _ _ _ Magnetic field lines

Figure from www.rfcafe.com



Waveguide Sizes and Frequency Ranges

VDI Designation	Internal Dimensions (µm)		Cut-off frequency	Suggested min.	Suggested max.	Calculated Loss (dB/cm) for Au *		Alternate	
	Width	Height	(ĠHz)	(GHz)	(GHz)	At min. frequency	At max. frequency	Designations	
WR-15	3759	1880	39.9	50	75	0.022	0.015	V	-
WR-12	3099	1549	48.4	60	90	0.030	0.020	Е	-
WR-10	2540	1270	59.01	75	110	0.039	0.027	W	-
WR-8.0	2032	1016	73.77	90	140	0.059	0.038	F	WR-8
WR-6.5	1651	825.5	90.79	110	170	0.081	0.052	D	WR-6
WR-5.1	1295	647.5	115.75	140	220	0.12	0.074	G	WR-5
WR-4.3	1092	546	137.27	170	260	0.14	0.1	-	WR-4
WR-3.4	864	432	173.49	220	330	0.2	0.14	-	WR-3
WM-710 (WR-2.8)	710	355	211.12	260	400	0.28	0.18	-	-
WM-570 (WR-2.2)	570	285	262.98	330	500	0.37	0.25	-	-
WM-470 (WR-1.9)	470	235	318.93	400	600	0.5	0.34	-	-
WM-380 (WR-1.5)	380	190	394.46	500	750	0.67	0.47	-	-
WM-310 (WR-1.2)	310	155	483.54	600	900	0.95	0.64	-	-
WM-250 (WR-1.0)	250	125	599.58	750	1100	1.3	0.88	-	-
WM-200 (WR-0.8)	200	100	749.48	900	1400	2	1.2	-	-
WM-164 (WR-0.65)	164	82	914	1100	1700	2.6	1.7	-	-
WM-130 (WR-0.51)	130	65	1153	1400	2200	3.7	2.3	-	-
WM-106 (WR-0.43)	106	53	1414.1	1700	2600	5.1	3.2	-	-
WM-86 (WR-0.34)	86	43	1743	2200	3300	6.3	4.3	-	-

* Waveguide loss calculated according to IEEE P1785.1



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THz Waveguide Interface Standards

IEEE P1785: A New **STANDARD FOR WAVEGUIDE** Above 110 GHz

The Microwave Theory and Techniques Society (MTT-S) of the IEEE has recently launched an activity to develop an international standard to define waveguides used at frequencies of 110 GHz and above-specifically, rectangular metallic waveguides. The standard's Working Group (P1785) has already met several times and is looking to define both the dimensions of the waveguides (and associated frequency bands) and their interfaces (that is flanges).

- Three proposed parts to the standard
 - Part 1: Define waveguide dimensions and associated frequency bands
 - Part 2: Define waveguide interfaces (i.e. flanges)
 - Part 3: Recommendations for Interface Performance and Uncertainty Specifications
- Part 1 is published and Part 3 is approved
- Part 2 still under development
- See http://grouper.ieee.org/groups/1785/



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CABLES & CONNECTORS SUPPLEMENT

TABLE III							
EXTENDED FREQUENCY BANDS AND WAVEGUIDE DIMENSIONS FOR THE IEEE STANDARD							
Waveguide Name Aperture Width (pm)		Aperture Height Cut-off Frequency (pm) (GHz)		Minimum Frequency (GHz)	Maximum Frequency (GHz)		
WM-71	71	35.5	2111.2	2000	4000		
WM-57	57	25.5	2629.7	3300	5000		









"flanges". The Working Group is keen to ensure that it considered all flange lesigns that are used regularly at hese frequencies (that is at 110 GHz nd above). Therefore, a subgroup is

being set up to investigate this matter further. Advice is also being sought from the entire millimeter- and submillimeter-wave communities to help identify any such candidate flange dedesign that you consider should be in-cluded in this standard, please contact the authors of this article. The plan is that the standard, when published, will contain all appropriate flanges that will be used routinely in this frequency region.

For example, one such flange that Nick Bidler and Box Giuley are chair and vice-chair, respective-ly, of the EEE P1785 working group is likely to be considered for inclu-sion in the standard is a precision ver-sion of the MIL-F-3922-67D flange (often called UG-387) that has been described⁵ and is shown in Figure 1. Compared to the conventional UG-387 flange,⁶ this precision version contains two additional alignment wards Rander, R.A. Ginley, J.L. He Korr, R.D. Pollard and D.F. Wills, wards Standardsoxi Wasescode 9

dowel holes immediately above and dover hores immediately above and below the waveguide aperture. These additional holes (and the associated dowel pins) are specified to a tighter dimensional tolerance than the dowel holes and pins found on the conven-tional UG-387 finge. This leads to hoters exchanged althought of the 23-25 March 2010. MIL-DTL-85/3C, "W angolar (Millio 2006. 2008. IEC 60153-2, "Hollow Metallic Wavegu Part 2: Relevant Specifications for Rectargular Wasseguides," Second Editio better mechanical alignment of the L. Hesler, A.B. Kerr, W. Grammer and I waveguide interfaces and hence lower

CONCLUSION

The IEEE is well on its way to pub-lishing a standard for defining rectan-

gular metallic waveguides for use at frequencies above 110 GHz. Already,

for the use of this part of the electro

magnetic spectrum-millimetre-wave

submillimeter-wave, terahertz, etc. Therefore, the publication of this stan-

dard is timely, and should serve our in dustry well for many years to come.

there are many applications emerging

of flanges. Another type of flange that is Another type of nange that is likely to be considered for inclusion in the standard is a newer design— a ring-centered flange,⁷ as shown in Figure 2. This design is compatible with both the UG-387 and preci-sion UG-387 flange designs, but also uses a coupling ring to significantly improve the alignment of the flange erfaces.

electrical reflection from a mated pair

ceinber 2009. H. Li, A.R. Kerr, J.L. Heiler, G. Wu, Q. Y N.S. Borber and B.M. Weikle H, "An In It is expected that the IEEE stan-dard, when published, will contain woved Ring-or Willingter an several flange designs, allowing endusers (such as customers, suppliers, etc.) to chose a design that best meets their given requirements. The role of and T.H. Chang, at DARES, Trans the standard in this context, is to pen-"2010 IEEE MTT-S Is vide the information needed for this choice to be made reliably.

CABLES & CONNECTORS SUPPLEMENT # MARCH 201

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Virginia Diodes Synthesizer Extenders



- WR-3.4 (220-330 GHz) Frequency Extender for Synthesizers
 - Tunerless, instantaneous sweeping over > 40% bandwidth
- AM modulation and Power Control capability
 - Voltage controlled
 - Can also be controlled by drive synthesizer





Virginia Diodes Synthesizer Extenders

- Low Drive for use with <20 GHz sources
- High Drive improved harmonic performance







VDI Amplifier/Multiplier Chain (AMC) Standard Product List						
VDI Dout #	Band (GHz)	BF Input Mode	Mult.	Output Power (dBm)		
VDI Part #			Factors	Typical	Minimum	
	750 1 100	Standard	81	22	.22	
WRI.0AMC	750 - 1,100	High	27	-23	-00	
	500 - 750	Standard	54	_21	-30	
WHT.SAMO	500 - 750	High	18	-21		
WR2.2AMC	225 - 500	Standard	36	-10	-19	
	325 - 500	High	12	-10	-10	
	260 - 400	Standard	24	6	-12	
WH2.8AWC		High	12	-0		
	220 - 330	Standard	18	-2	0	
WR3.4AMC		High	9		-0	
WP4 24MC	170 - 260	Standard	18	2	-5	
WH4.SAMO		High	6	2		
WR5.1AMC	140 220	Standard	12	1	0	
	140 - 220	High	6	4		
WR6.5AMC	110 - 170	Standard	12	0	2	
		High	4	0		
WR8.0AMC	90 - 140	Standard	3	0	3	
		High	9	9		
WR9.0AMC	82.5 125	Standard	9	14	10	
	02.0 - 120	High	3	14		
WRIDAMC	75 - 110	Standard	6	14	10	
WHIDAMC	75-110	High	3	14		
	10 110	High	3	17		



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Virginia Diodes Spectrum Analyzer Extenders



- Fullband down-conversion and frequency extension of microwave spectrum analyzers into the THz range
 - Coverage from 75GHz-1,100GHz
 - IF Bandwidth to 40 GHz
 - Turnkey operation





LO Inpu

Virginia Diodes Spectrum Analyzer Extenders

- State-of-the-Art Sensitivity
- Displayed Average Noise Level (DANL)
 - A measure of the minimum detectable signal with 1 Hz bandwidth

VDL Dort #	RF Band	SSB Conversion Loss (dB)	Displayed Average		
VDI Pall#	(GHz)	Intrinsic Mixer**	Noise Level (dBm/Hz)*		
WR1.0MixAMC	750 - 1,100	30	-135		
WR1.5MixAMC	500 - 750 -	20	-150		
WR2.2MixAMC	325 - 500 ·	17	-150		
WR2.8MixAMC	260 - 400 ·	15	-150		
WR3.4MixAMC	220 - 330 -	14	-150		
WR4.3MixAMC	170 - 260 -	14	-150		
WR5.1MixAMC	140 - 220 -	12	-150		
WR6.5MixAMC	110 - 170 -	12	-150		
WR8.0MixAMC	90 - 140	12	-150		
WR10MixAMC	75 - 110	11	-150		



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Virginia Diodes Spectrum Analyzer Extenders

 Extender can be reconfigured by the user depending upon the measurement requirements



VDI MixAMC Setup for Block Downconversion



VDI MixAMC Setup for Spectrum Analyzer Extension





Block Down Conversion



MixAMC & Spectrum Analyzers: Block Downconversion

- General principles of Block
 Downconversion
 - MixAMC is driven by external synthesizer, and a block of RF signals are downconverted and fed into the Spectrum Analyzer (SA)
 - RF signals (both upper and lower sideband) are downconverted to IF
 - External synthesizer fixed while SA sweeps over its range
 - RF coverage limited by IF bandwidth of mixer (or SA maximum frequency)
 - Maximum IF ranges from 8 GHz up to > 40 GHz, depending upon the waveguide band
- Uses of block downconversion
 - General analysis of THz signals
 - Requires User analysis
 - Can be used for signals that drift, or for wideband communication signals
 - The THz signal is reproduced at the IF by heterodyne mixing process
 - e.g. can be used in a communication system, spectral information is preserved



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Spectrum Analyzer Display

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MixAMC & Spectrum Analyzers: Frequency Analyzer Extension

- General principles of Spectrum Analyzer Extension
 - MixAMC drive by LO signal from Spectrum Analyzer
 - Swept across full band of mixer
 - RF coverage set by mixer RF bandwidth
 - Full waveguide band systems available (> 40% BW)
- Uses of Frequency Analyzer
 Extension
 - General signal analysis
 - Signal identification used to determine the actual frequency of the RF signal and remove spurious signals
 - Signal ID of limited use for drifting signals
 - e.g. banded communication signal or free-running oscillator
 - Spectral information won't be preserved to time variant signals
 - Conversion loss table used to adjust power level



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Spectrum Analyzer Display



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Demonstration of Signal Analysis

- Use VDI MixAMC to extend a microwave spectrum analyzer to 500-750 GHz
- Test the harmonic purity and phase noise of VDI 500-750 GHz source





Spectral purity of a 625 GHz Signal

- Measurement of 625 GHz VDI source
- All signal are harmonically related to microwave drive synthesizer
 - Harmonics more than 20 dB down from carrier
 - No spurious (i.e. non-harmonic) signals present





Phase Noise Measurement at 700 GHz

- Phase noise follows the theoretical 20*log(N) behavior
 - No excess phase noise added by source





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Virginia Diodes VNA Extenders

- VDI Extenders from WR-10 (75-110 GHz) thru WM-250 (750-1100GHz)
 - State-of-the-art Dynamic range
 - 120 dB (typ.) at WR-10 (70-110 GHz)
 - 120 dB (typ.) at WR-5.1 (140-220 GHz)
 - 100 dB (typ.) at WM-380 (500-750 GHz)
 - 70 dB (typ.) at WM-250 (750-1100 GHz)
 - Excellent amplitude and phase stability
 - Fully calibrated measurements



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VNA Extender Diagram

Full TxRx Extender





WM-250 VNA Extender

- Dynamic Range: 60 dB typical at 10Hz BW
- Dynamic Range: 40 dB minimum at 10Hz BW
- Magnitude Stability: ±1 dB
- Phase Stability: ±15°
- Test Port Power: -35 dBm
- Test Port Input Limit (dBm, saturation/damage): -20/13
- Directivity: 30 dB
- Typical Dimensions: 8 x 5 x 3 inches







WM-250 – Amplitude & Phase Stability

- Look at amplitude & phase stability of system over one hour
 - Stability is important to maintain the calibration during the measurements
 - Measured for full 2-port WR-1.0 extender
 - 1-port stability typically 5-10 times better
- Stability was measured in general laboratory space
 - Poorly controlled thermal environment
 - Significantly improved performance can be achieved in a controlled thermal environment





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THz Waveguide Calibration

- mm-Wave waveguide calibration methods
 - Short-Open-Load-Thru (SOLT, TOSM)
 - Open typically uses 1/4-wave delayed short
 - Thru-Reflect-Line (TRL, LRL)
 - Line is typically a 1/4-wave thru shim
 - Many others possibilities as well...
- Sub-mm wave introduces a new set of challenges
 - Thru-Reflect-Line (TRL, LRL)
 - ¼-wave shims difficult to fabricate and fragile
 - Common to instead use two lines with ¼-wave difference in length
 - However, this means more connections and interfaces () less accuracy
 - Short-Open-Load-Thru (SOLT, TOSM)
 - Challenging to achieve a high return loss load



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Machined Quarterwave Delay Short



WM-380 Precision Loads



WM-250 Calibrated Measurements

- Calibrated measurements were performed using the Extender
- Short-Open-Load-Thru calibration method
 - 1/4-wave delay was used as the Open standard
- 1 kHz IF Bandwidth for calibrated measurements

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Measurement of 1" Waveguide Straight

Measurement of Waveguide Attenuator

One-Port Quasi-Optical Measurement Setup

One-Port Quasi-Optical Measurements

1-Port Measurement in Focused Beam

- Requires large sample
- Sample in collimated beam

- Can use small sample
- Good for devices (grid arrays, focused optics, ...)

Quasi-Optical Grid Array Sideband Generator

1.6 THz 100 Element Diode Array

100 Element Diode Array for Wavefront Modulation

University of Virginia

Quasi-Optical Measurement Calibration

Measurement of Sample in Focused Beam

- Slide lens and sample as a unit
 - Translation occurs in collimated section
 - Improved accuracy, minimal effect on focusing
 - e.g. see Arsenovic 2013 MTT
 - Measure multiple delay lengths

One-Port Quasi-Optical Measurement Setup

Quasi-Optical Measurement Setup

Over-Determined Least Squares Calibration

- For calibration, use an un-weighted least squares method
 - e.g. see Wong 2004 ARFTG
- Calibration standards
 - Series of delayed reflections with known delay distances
 - Metal plate at focal point of QO system
 - Metal plate and focusing mirror are both mounted on the same moving stage
 - Matched load
 - Used absorber at 45 degree angle as rough termination
 - Measurement bandwidth 300 Hz

Over-determined Least Squares Calibration

Uncertainty Analysis of the Weighted Least Squares VNA Calibration

Ken Wong, Senior Member IEEE, Agilent Technologies, Inc.

64th ARFTG Conference

B. Least Squares solution

Better accuracy can be achieved by measuring more than three standards. Using n calibration standards, equation (3) becomes:

$$\begin{bmatrix} \mathbf{1} & \Gamma_{m1}\Gamma_{a1} & -\Gamma_{a1} \\ \mathbf{1} & \Gamma_{m2}\Gamma_{a2} & -\Gamma_{a2} \\ \mathbf{1} & \Gamma_{m3}\Gamma_{a3} & -\Gamma_{a3} \\ \vdots & \vdots & \vdots \\ \mathbf{1} & \Gamma_{mn}\Gamma_{an} & -\Gamma_{an} \end{bmatrix} * \begin{bmatrix} e_{00} \\ e_{11} \\ \Delta_e \end{bmatrix} = \begin{bmatrix} \Gamma_{m1} \\ \Gamma_{m2} \\ \Gamma_{m3} \\ \vdots \\ \Gamma_{mn} \end{bmatrix}$$
(5)

Equation (5) can be rewritten as a linear matrix equation:

$$A \cdot E = M \tag{6}$$

The least squares solution to equation (6) is given as:

$$E = \left(A^H \cdot A\right)^{-1} \cdot A^H \cdot M \tag{7}$$

where A^{H} is the conjugate transpose of A.

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Evaluation of Calibration Quality

- Look at Sparameters of the calibration standards
 - Over-determined calibration → a measure of the calibration quality
- Gives an indication of the measurement quality that can be achieved

Evaluation of Calibration Quality

Evaluation of Calibration Quality - Shorts

S-Parameters of Quasi-Optical System

- A measurement of the S-parameters of the Quasi-Optical system
- Measured using a two-tiered extraction method
- Uses a wavequide calibration followed by a separate QO calibration
 - See Arsenovic 2013 MTT
- Vector Star has onboard two-tiered calibration available
 - Network Extraction

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Atmospheric Transmission

Measurements of Dielectric Samples

- Samples were taped to the metal plate at the focal point
- Repeated measurements were made of each sample
 - Sample removed from plate and re-mounted for each measurement
- Calibration using the QO method described earlier
 - Not a two-tiered calibration

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THz Wafer Probing

- Rapid advances in InP THz transistors
 - NGC has developed a 650 GHz amp with > 10 dB gain and P_{SAT} of 1.7 mW
 - Radisic MTT 2012
- The VDI THz VNA Extenders are use for on wafer probing of these THz transistors
 - Rapid device characterization (no fixture de-embedding)

480 GHz LNA (NGC, Deal – MWCL - 2010)

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Dominion MicroProbes, Inc. Charlottesville, VA www.dmprobes.com sales@dmprobes.com (434) 962-8221

500-750 GHz Wafer Probes

- WR1.5 Probes with replaceable single chip construction
- Average insertion loss of 7-8 dB
- Average return loss > 10 dB
- Excellent repeatability and durability
- Compatible with VDI WR-1.5 flanges

WM-380 Micromachined Probes – RF Performance

TRL Measurements from Northrup Grumman

Images courtesy of W.R. Deal

World's first TRL calibration above 500 GHz!
 UVa wafer probes with VDI THz Extenders

• The probe design is being extended to 1.1 THz for use with VDI 1.1 THz extenders

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Recent Development: Mini-Modules

Full TxRx – 1.5" x 3" x 8.5"

Stand-alone Rx – 0.75" x 1" x 2.5"

High Dynamic Range Transceivers

- VDI has developed a series of extended dynamic range transceivers
 - Customized for applications requiring high dynamic range, e.g. antenna testing
 - For use with DUTs with high loss
 - e.g. at WR-3.4 (220-330 GHz) a dynamic range of 120 dB can be achieved for DUT with 20 dB loss
 - Measurement mixer will be compressed at low bands by direct connection
- The system architecture is simplified from a typical VNA extender
 - Consists of a Source with Reference Mixer and a Measurement Mixer
 - Typical configuration for antenna testing

Conclusions

- VDI Goal: Open the THz window for routine technological use
- Technology based on Schottky diodes.
- Keys to success include innovative circuit designs, modern CAD, and advanced fabrication technology.
- Source power and frequency continues to increase.
- High performance, manufacturable systems have been developed
 - Custom sources and receivers are available at any frequency from 50 GHz through 3.1 THz
 - Full-waveguide band frequency extenders for
 - Signal generators
 - Spectrum analyzers
 - Network analyzers
- Higher levels of integration are allowing the development of more compact systems.

